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# **Stormwater Management Plan**

Wickham Woolstores

3rd July 2017

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## **Issue and Revision Record**

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# 1 Introduction

Mott MacDonald (MM) has been commissioned by Investec Australia Limited to prepare a water cycle management plan for the proposed mixed-use urban domain at Wickham Woolstores. This report will be lodged with Newcastle City Council to support the Development Application (DA). The report details the modelling, procedures and results obtained in developing the water cycle management plan for the site.

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## 1.1 Objectives

This report was prepared by MM and details the procedures and results from analysis undertaken in developing the stormwater management strategy for the Wickham Woolstores development in Newcastle. It supports the masterplan by providing engineering input with respect to an integrated approach to flood risk management and water sensitive urban design (WSUD).

## 1.2 Scope of Work

The purpose of the analyses was to:

- Undertake a hydrologic, hydraulic and water quality assessment of the proposed development as an integrated approach to flood risk and stormwater management;
- Design a pit and pipe network with necessary discharge controls to restrict the developed flows to the existing flows;
- Design a water quality treatment train to address the pollution reduction targets set out by Newcastle City Council; and
- Undertake a flooding desktop assessment to demonstrate that proposed developments are compliant with Council standards and current Flood Certificate.

The following methodology has been adopted to assess the above scope of work:

- Collate the existing site data;
- Review design controls and requirements set out by Newcastle City Council;
- Undertake a hydrologic catchment analysis to compare existing site flows to proposed developed flows and determine stormwater detention strategies;
- Assess the impact the proposed development has on regional water quality and develop water quality treatment strategies; and
- Undertake hydraulic modelling to assess the impact the proposed development has on surrounding environs and determine appropriate modifications required to minimise the impact on surrounding land.

## **1.3 Civil Engineering Documentation for Development Application**

The following drawings have been prepared as part of the civil engineering documentation for development application:

DA-1001 - Cover Sheet

DA-1002 - General Notes Sheet

DA-1003 - Legends Sheet

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- DA-1010 General Arrangement Plan
- DA-1012 Siteworks Grading Plan Sheet 1
- DA-1013 Siteworks Grading Plan Sheet 2
- DA-1014 Siteworks Grading Plan Sheet 3
- DA-1015 Siteworks Grading Plan Sheet 4
- DA-1016 Siteworks Grading Plan Sheet 5
- DA-1020 Typical Road Cross Sections Sheet 1
- DA-1021 Typical Road Cross Sections Sheet 2
- DA-1030 Soil and Water Management Plan
- DA-1035 Soil and Water Management notes and Details
- DA-1040 Stormwater Management Plan Sheet 1
- DA-1041 Stormwater Management Plan Sheet 2
- DA-1042 Stormwater Management Plan Sheet 3
- DA-1043 Stormwater Management Plan Sheet 4
- DA-1044 Stormwater Management Plan Sheet 5
- DA-1050 Road Longitudinal Sections Sheet 1
- DA-1051 Road Longitudinal Sections Sheet 2
- DA-1060 Siteworks and Stormwater Drainage Details Sheet 1
- DA-1061 Siteworks and Stormwater Drainage Details Sheet 2
- DA-1070 Above Ground Detention Basin Plan and Section

## **2** The Physical Environment

## 2.1 The Site

The subject site (Figure 1) is located approximately 5km northwest of Newcastle CBD on Lots 1 – 3 DP346352 and Lot 13 DP830026. The site is bound by The Avenue to its north, Milford Street to its west and Annie Street to its south. It is also directly adjacent to the Caltex Oil Terminal on its northern and eastern boundary.

The site falls within the Newcastle City Council Local Government Area (LGA) and has an area of approximately 3 ha. The existing site is dominated by three (3) mid-20<sup>th</sup> century heritage listed Woolstores, which have laneways running between them. They are four (4) storeys with concrete framed brick facades, internal timber framing and floors with sawtooth roofs. Bridge additions link the buildings at upper levels across the laneways. The buildings currently contain low-intensity light industrial uses, such as storage and artists' studios.



#### Figure 1: Site Location

Source: Six Maps NSW

## 2.2 Proposed Site Layout

The proposed development is a mixed-use development including five (5) mixed-use buildings and a large recreational park to the northern section of the site. Woolstores 1, 2 and Building 5 are residential buildings with internal car parking. Woolstore 3 is mixed use with residential where light amenity is high, retail to ground floor areas and car parking to the interior. Commercial uses take up the remainder of the available Woolstore 3 space. Similarly, Building 4 is a mixed-used building for both retail and artisan production community.

Please refer to Table 1 and Figure 2 below for the preferred masterplan option and an indicative building summary.

Building	Apts	Residential Area (GFA)	Retail & Production Area (GFA)	Commercial & Community Area (GFA)	Total GFA	Total Gross Building Area
Woolstore 1	100	11875	0	0	13535	18538
Woolstore 2	99	11875	0	0	11875	18538
Woolstore 3	42	4496	820	5746	11062	17628
Building 4	0	0	1651	2858	4509	7805
Building 5	69	9907	170	0	10077	17224

2641

8604

51058

79733

#### **Table 1: Building Summary**

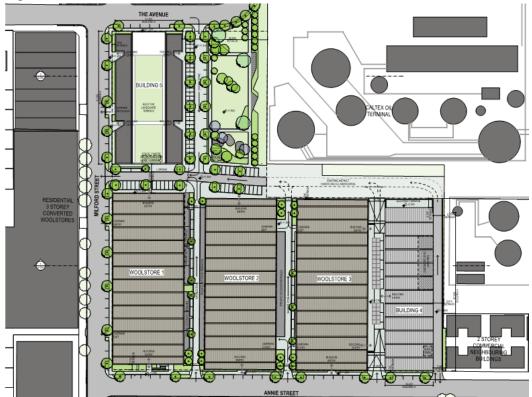
310

Source: Prepared by Tonkin Zulaikha Greer, Fairweather Jemmot & City Plan Services, Dated 27/06/2017

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#### Figure 2: Site Plan

**Total Summary** 

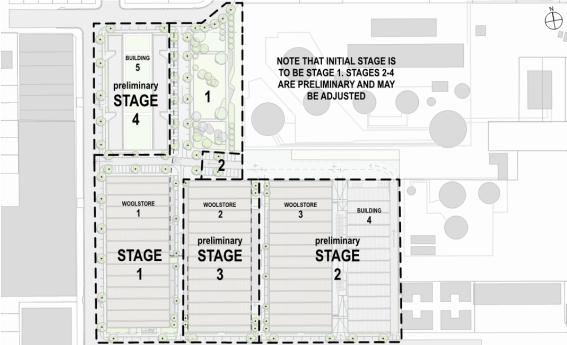


Source: Prepared by Tonkin Zulaikha Greer, Site Plan, Dated 25/06/2017

Note that a staged approach is adopted for the proposed development at Wickham Woolstores. The initial stage is to be stage 1 including the construction of Woolstore 1 and a recreational park whereas stages 2 - 4 are preliminary and subject to future refinement.

Please refer to Figure 3 below for the staging plan for Wickham Woolstores.





Source: Prepared by Tonkin Zulaikha Greer, Staging Plan, Dated 25/06/2017

## 2.3 Site Grading

The proposed site grading has been undertaken to drain the site to its north towards The Avenue and to its south towards Annie Street. The design intention is to ensure the existing pipe capacity downstream of the proposed development is not undermined.

The pit and pipe network has been designed to intercept the flows, ensuring safe overland flow conveyance in the dish drains, and to divert the majority of the site flows towards the on-site detention basins if applicable.

The grading has been undertaken with consideration to optimise the future earthworks and provide flood protection freeboard to the proposed residential buildings.

The proposed grading has been designed to match the existing levels of The Avenue, Milford Street and Annie Street.

#### 2.4 Pavements

The internal site pavement has been provided as per Landscape Layout. Please refer to drawings MMD-366163-C-DR-00-DA-1030 – 1034 for the proposed pavement layout in Wickham Woolstores.

The pavement profile is subject to future refinement at detailed design stage once the geotechnical information becomes available.

## 2.5 Soil and Erosion Control during Construction

As indicated on the Concept Soil and Water Management Plans MMD-366163-C-DR-00-DA-1020 – 1021, several control measures are proposed during the construction to manage soil and erosion runoff on-site. The control measures will be confirmed by the construction contractor and are likely to include:

- Temporary sediment fencing at the site boundary;
- Temporary sandbag sediment traps around kerb inlet pits;
- Temporary geotextile filter fabric sediment traps around surface inlet pits and junction pits;
- Temporary maintained site access; and
- Temporary sediment basins.

## 2.6 Stormwater Management

As part of the DA documentation, a MUSIC and a DRAINS model have been included to ensure the stormwater design is compliant with Newcastle City Council's requirements.

This report will assess the stormwater modelling and design control requirements in detail in the following sections. The pit and pipe network (the minor system) was designed to cater for the 20-year ARI event without creating significant ponding or flows in traficable areas, where as the major system is designed to the 100-year ARI to allow for overflows in extreme events to convey stormwater to the dsicharge point of the site.

## 2.7 Utility Services

Utility services including sewer, potable water, gas, telecommunications and electrical will be documented in the detailed design stage for the proposed development. At this stage, we have identified the potential conflicts between the proposed stormwater infrastructure and the existing utilities in the street. Further investigation is to be undertaken during detailed design stage.

## **3 Design Controls**

This Stormwater Management Report was prepared in conjunction with relevant standards and requirements of various agencies. The documents used as part of the design control are detailed within this section.

#### 3.1 Australian Rainfall and Runoff – Volume 1 (2001)

Prepared by the Institution of Engineers, Australia Australian Rainfall and Runoff – A Guide to Flood Estimation was written to "provide Australian designers with the best available information on design flood estimation". It contains procedures for estimating stormwater runoff for a range of catchments and rainfall events and design methods for urban stormwater drainage systems.

#### 3.2 Newcastle City Council Control Documents

#### 3.2.1 Newcastle Development Control Plan 2012

The *Newcastle Development Control Plan (DCP) 2012* provides the necessary controls for the redevelopment of the site. This DCP provides detailed provisions relating to matters of significance to the City of Newcastle to be considered by Council.

As part of the DCP, Section 7.06 provide detailed stormwater controls for the following:

- Stormwater collection;
- Flooding and runoff regimes;
- Storage;
- Storage drawdown;
- Site discharge controls;
- Pollutants;
- Overflow disposal;
- Existing drainage systems; and
- Installation and maintenance requirements.

#### 3.2.2 Council's Technical Manual – Stormwater and Water Efficiency for Development

In conjunction with Council's DCP, Council's Technical Manual sets out the requirements for the design of stormwater drainage for urban and rural areas. The manual outlines a broad strategy of the design and development of land within the Newcastle local government area, including:

- Stormwater collection;
- Site discharge controls large scale development; and
- Overflow disposal.

## 4 Water Quantity Modelling

The assessment of water quantity was completed through hydrological modelling. Computerbased models of the existing and developed catchments were constructed using DRAINS. Design storms were applied to these models to give estimates of the 1, 2, 5, 10, 20 and 100year ARI discharges which are examined in the following sections. Assessment of these models then allowed the sizing and configuration of a proposed detention basin and the documentation of their requirements.

## 4.1 **DRAINS Parameters**

#### 4.1.1 Hydrological Model

In order to assess the performance of the proposed pit and pipe network, the following Hydrological Model has been established in Table 2.

#### **Table 2: Hydrological Model Specification**

Item	Input
Paved (Impervious) Area Depression Storage	1 mm
Supplementary Area Depression Storage	0 mm
Grassed (Pervious) Area Depression Storage	5 mm
Soil Type	3

Note that type 3 (or type C) soil is defined in DRAINS as the soil with slow infiltration rates.

### 4.1.2 Rainfall Data

According to Figure 3.2 of ARR87, the proposed development is situated within Zone 2 – Murray Darling with Antecedent Moisture Condition (AMC) is 3. Please find below definitions of AMC value and its relationship to rainfall storage in Table 3.

#### **Table 3: Antecedent Moisture Condition**

Description	Total Rainfall in 5 days preceding the storm (mm)
Completely Dry	0
Rather Dry	0 to 12.5
Rather Wet	12.5 to 25
Saturated	Over 25
	Completely Dry Rather Dry Rather Wet

Source: DRAINS Manual

A AMC value of 3 means that the moisture content of the soil is higher and will generate higher runoff rates due to lower infiltration. This is set up to provide a more conservative approach to the hydraulic design.

### 4.1.2.1 Intensity-Frequency-Duration (IFD)

IFD data is obtained from Council's Technical Manual Appendix 1. Design storms events selected for DRAINS modelling include 1, 2, 5, 10, 20, 50 and 100 years. Please find DRAINS inputs in Table 4.

Duration	1 Year	2 Year	5 Year	10 Year	20 Year	50 Year	100 Year
5 mins	85.51	109.9	141.42	158.38	181.93	212.69	236.05
10 mins	65.52	84.27	108.65	121.8	140.03	163.86	181.98
15 mins	54.73	70.44	90.93	102.01	117.34	137.4	152.65
20 mins	47.68	61.38	79.32	89.03	102.46	120.03	133.4
25 mins	42.6	54.86	70.95	79.67	91.72	107.49	119.5
30 mins	38.73	49.89	64.56	72.52	83.52	97.91	108.88
45 mins	31.04	40	51.86	58.3	67.19	78.83	87.7
60 mins	26.35	33.98	44.1	49.61	57.2	67.15	74.74
90 mins	20.49	26.43	34.34	38.65	44.58	52.36	58.29
2 hours	17.08	22.04	28.65	32.25	37.22	43.73	48.69

#### Table 4: IFD Data

Source: Newcastle City Council's Technical Manual Appendix 1

#### 4.1.3 Major and Minor Design Storm

The water quantity was modelled in relation to the requirements of Newcastle City Council's Technical manual in conjunction with Section 7.06 Stormwater. The following criteria were considered in the modelling and design process:

- The piped drainage is to be designed for the minor system 20-year ARI storm event; and
- Detention is required to attenuate flows where the developed flows are in excess of natural flows. The detention is to be designed to perform in the full range of flood events up to the 100-year ARI storm event.

#### 4.1.4 Hydraulic Roughness Parameters

Manning's values were applied to the model based on pipe material used. A manning's 'n' of 0.013 was applied to all reinforced concrete pipes.

#### 4.1.5 Pipes

Proposed pipes were graded at a minimum slope of 1% for pipe diameters up to 150mm and 0.5% for diameters of 225mm and larger. Based on Council's standard drawings A200, a desirable minimum cover of 400mm over the pipe is required, concrete encasement of pipe work is to occur under all pavement where minimum required cover cannot be achieved.

#### 4.1.6 Overland Flow Paths

Typical cross-sections based on the gutter shape and pavement type were input to DRAINS representing the overland flow paths. Slopes were derived from the proposed pit surface levels.

#### 4.1.7 Tailwater Levels

Newcastle City Council has no information available regarding tailwater levels of the existing stormwater pits in the street. In this regard, the following assumptions have been made for the civil design:

- Tailwater level for 100 year is 150mm above the surface level of the existing pit;
- Tailwater level for 50 year is 75mm above the surface level of the existing pit;
- Tailwater level for 20 year is at the surface level of the existing pit;
- Tailwater for 10 year is 75mm below the surface level of the existing pit; and
- Tailwater levels for 1, 2 and 5 year are 150mm below the surface level of the existing pit.

## 4.2 Existing Scenario

#### 4.2.1 Existing Catchment

The total catchment area being conveyed downstream to the site in the current scenario is approximately 3 ha. Based on the detailed survey prepared by Monteath & Powys, the existing project site can be divided into two (2) catchments, the Northern and the Southern.

In addition, upstream catchments have also been identified within the adjacent easement that is generating additional stormwater runoff through the site. According to the survey, the easement is designated for construction a street or railway line benefiting the project site (Lots 1, 2 and 3 DP346352).

Figure 4 indicates the existing catchment plan and direction of flows whereas Table 5 summarizes the existing catchment conditions.



#### Figure 4: Existing Catchment Analysis

Catchment	Sub-catchment	Area (sqm)	% of Impervious
	1	96.26	17%
	2	3285.69	100%
Northern Catchment	3	1993.36	97%
	4 (Bypass)	1306.70	97%
	Sub-total	6682.00	97%
	5	11348.89	99%
	6	6334.67	100%
Southern Catchment	7	7561.30	94%
	8 (Bypass)	402.08	15%
	Sub-total	25646.94	96%

### **Table 5: Existing Catchment Analysis**

## 4.2.2 DRAINS Results for Existing Scenario

The existing scenario DRAINS model was built using the parameters specified in Section 4.1 of this report.

The discharge rates in Table 6 were computed for the 20-year ARI (minor) and 100-year ARI (major), as per Newcastle City Council's Technical manual.

#### **Table 6: Existing Scenario Discharge Rates**

Storm Event	Discharge Rate (m³/s)			
Storm Event	Northern Catchment	Southern Catchment		
Minor (20-year ARI)	0.33	1.26		
Major (100-year ARI)	0.41	1.56		

## 4.3 Developed Scenario

According to Newcastle City Council's standards, the stormwater runoff generated from the proposed development needs to be managed to ensure downstream drainage systems are not compromised. Analysis has been undertaken to identify the need of stormwater detention on-site.

### 4.3.1 Developed Catchment

Based on the Architectural layout prepared by Tonkin Zulaikha Greer Architects and Fairweather Architecture, Figure 5 indicates the proposed catchments for the subject site. Please find a summary of proposed catchment conditions in Table 7.

A strip of grated drains is to be provided at the eastern and southern boundaries of the easement area to prevent surface stormwater bypass. Note that the current sitework gradings were designed to meet the existing levels along The Avenue, Milford Street, Annie Street and the existing easement.



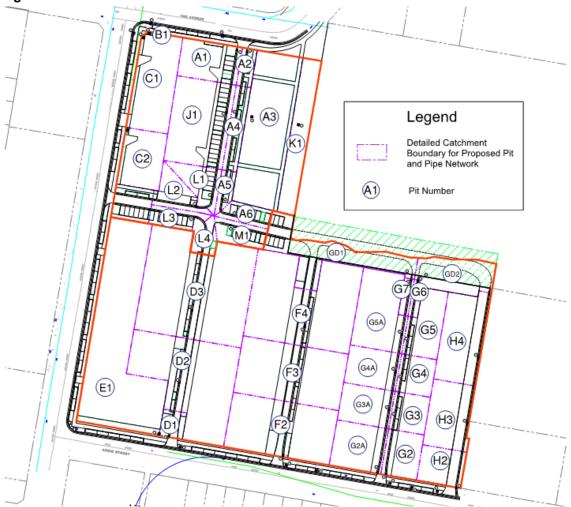
#### Figure 5: Proposed Catchment Analysis

Catchment	Sub-catchment	Area (sqm)	% of Impervious
	1	14.58	0%
	2	7289.57	61%
Northern Catchment	3	1776.29	94%
	4 (Bypass)	353.15	84%
	Sub-total	9433.58	68%
	5	10667.30	97%
Southern Catchment	6	5711.96	98%
Southern Catchment	7	6510.32	97%
	Sub-total	22889.58	97%

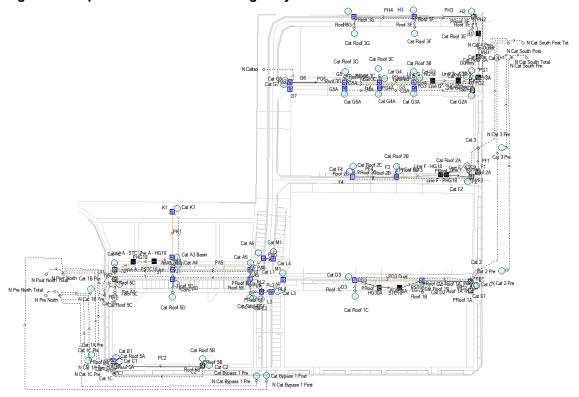
#### **Table 7: Proposed Catchment Analysis**

#### 4.3.2 DRAINS Results for Developed Scenario

The proposed pit and pipe network was designed to convey the 20-year ARI storm event using the DRAINS parameters specified in Section 4.1. A detailed catchment plan is shown in Figure 6 of the proposed stormwater drainage network. The layout of the developed scenario has been modelled in DRAINS as indicated in Figure 7.



## Figure 6: Detailed Catchment Plan



#### Figure 7: Proposed Stormwater Drainage Layout

The discharge rates in Table 8 were computed for the 20-year ARI (minor) and 100-year ARI (major), as per Newcastle City Council's Technical manual.

#### **Table 8: Developed Scenario Discharge Rates**

Storm Event	Discharge Rate (m³/s)			
Storm Event	Northern Catchment	Southern Catchment		
Minor (20-year ARI)	0.39	1.10		
Major (100-year ARI)	0.49	1.23		

Comparing to Table 6, the developed discharge rates in Northern Catchment appears to exceed those in the pre-development scenario and have the downstream pipe capacity undermined. In this regard, a site discharge control system is required to meet Council's requirements.

#### 4.3.3 Site Discharge Controls

A combination of measures was considered for the proposed development considering the constrains and opportunities presented on the project site. In general, an above-ground onsite stormwater detention (OSD) basin and rainwater tanks (RWT) are recommended to mitigate the excessive discharge rate.

#### 4.3.3.1 RWT

According to Newcastle City Council's DCP, it is recommended of using RWTs for residential development which the volume of the tank can be used to offset any additional discharge control storage that is required.

Based on the assessment undertaken by the project Hydraulic Engineer, RWTs are to be provided for each building within the project site. Table 9 summarizes the design parameters of RWTs which are subject to future refinement at detailed design stage.

### Table 9: RWT Design Parameters

<b>Proposed Development</b>	Roof Area (ha)	% of Roof Bypass	Indicative RWT Size (kL)
Woolstore 1	0.465	57%	40
Woolstore 2	0.465	57%	40
Woolstore 3	0.464	18%	65
Building 4	0.294	5%	55
Building 5	0.334	55%	65

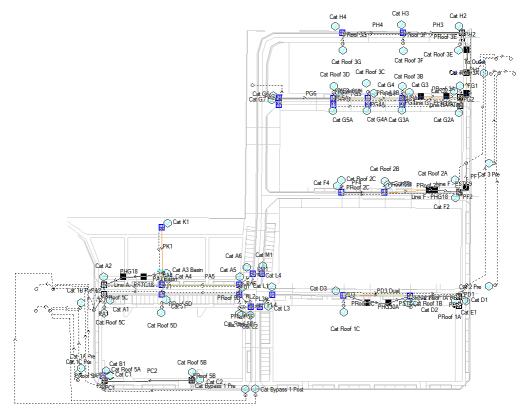
## 4.3.3.2 OSD

After offseting the volume of Building 5's RWT, an above-ground OSD basin with a totoal volume of 22 kL has been incorporated in the developed scenario. The basin is considred to be placed within the recreational park situated within the Northern catchment.

## 4.4 DRAINS Results for Developed Scenario with Discharge Controls

The layout of the modified DRAINS model is shown below in Figure 8 whereas the discharge rates have been summarized in Table 10.

## Figure 8: Modified DRAINS Layout



#### Table 10: Modified Scenario Discharge Rates

Storm Event	Discharge Rate (m³/s)								
Storm Event	Northern Catchment	Southern Catchment							
Minor (20-year ARI)	0.19	1.10							
Major (100-year ARI)	0.23	0.23							

Compared to existing scenarios, the discharge rates of the modified stormwater drainage layout appears to be satisfactory.

DRAINS input data and results are attached in Appendix A for reference.

## 5 Water Quality Modelling

Treatment removal loads were analysed from existing to developed scenarios using MUSIC (Model for Urban Stormwater Improvement Conceptualisation) Version 6 software. MUSIC is a water quality modelling tool which was utilised to simulate urban stormwater systems operating at a range of temporal and spatial scales.

## 5.1 Stormwater Quality Targets

Newcastle City Council has established the water quality targets as indicated in Table 11.

#### Table 11: Newcastle City Council Water Quality Targets

Pollutant	% Reduction in Pollutant Loads
Gross Pollutants (>5mm)	90%
Total Suspended Solids	85%
Total Phosphorus	65%
Total Nitrogen	45%

The above objectives are expressed as the reduction in pollutant loads required.

## 5.2 MUSIC Model Parameters

## 5.2.1 Rainfall Data

The water quality analysis requires historical rainfall data recorded by a pluviograph station. As requested in Council's DCP, the modelling is to be undertaken at a 6-minute time step using Williamstown pluviograph station over the time period 1/1/2002 - 31/12/2006.

#### 5.2.2 Soil Store Parameters

The soil store parameters used within the model were based on the *Draft NSW MUSIC Modelling Guidelines,* as recommended in Council's DCP. Parameters used are summarised in Table 12.

#### Table 12: MUSIC Parameters – Soil Properties

Parameter	Unit	<b>Recommended Values</b>	Description
Impervious Area			
	_	0.3	Roofs
Rainfall Threshold	mm	1.5	Sealed roads, driveways, paving and paths
		1	For all land uses
Pervious Area			
Soil Capacity	mm	170	
Initial Storage	%	30	
Field Capacity	mm	70	For urban development
Infiltration Capacity Coefficient	а	210	
Infiltration Capacity Coefficient	b	4.7	

Parameter	Unit	<b>Recommended Values</b>	Description
Groundwater			
Initial Depth	mm	10	
Daily Recharge Rate	%	50	
Daily Baseflow Rate	%	5	For urban development
Deep Seepage	%	0	

Source: Draft NSW MUSIC Modelling Guidelines (August 2010)

#### 5.2.3 Pollutant Generation Parameters

The pollutant generation parameters used within the model were based on the *Draft NSW MUSIC Modelling Guidelines,* as recommended in Council's DCP. Parameters used are summarised in Table 13.

### Table 13: MUSIC Parameters – Pollutant Generation

Surface Type	Flow Type	т	SS	1	ſP	TN		
	гюм туре	Mean	Std Dev	Mean	Std Dev	Mean	Std dev	
Roof / Roof Bypass**	Base Flow	n/a	n/a	n/a	n/a	n/a	n/a	
RUUI / RUUI Dypass	Storm Flow	1.30	0.32	-0.89	0.25	0.30	0.19	
Sealed Roads	Base Flow	1.20	0.17	-0.85	0.19	0.11	0.12	
	Storm Flow	2.43	0.32	-0.3	0.25	0.34	0.19	
Londoconing	Base Flow	1.20	0.17	-0.85	0.19	0.11	0.12	
	Storm Flow	2.15	0.32	-0.60	0.25	0.30	0.19	

Source: Draft NSW MUSIC Modelling Guidelines (August 2010)

\*\*Note the base flow parameters are applied to groundwater flow, whist the storm flow parameters are applied to surface runoff. Base flow concertation parameters are not applicable to where surface is 100% impervious.

## 5.3 Developed Scenario

#### 5.3.1 Developed Catchment

Based on the landscape layout prepared by JMD Design, the proposed catchments have been further refined based on the surface type. Table 14 summarised the catchment analysis prepared for MUSIC.

#### Table 14: MUSCI Catchment Analysis

			Roo	f Area	Seale	d Road	Landscaping		
Catchment	Sub- catchment	Total Area (ha)	Total Area (ha)	% of Imperv	Total Area (ha)	% of Imperv	Total Area (ha)	% of Imperv	
	1	0.001	0.000	n/a	0.000	n/a	0.001	0%	
Northern	2	0.729	0.171	100%	0.207	85%	0.351	28%	
Catchment	3	0.178	0.163	100%	0.000	n/a	0.014	26%	
	4	0.035	0.000	n/a	0.028	79%	0.007	100%	
	5	1.067	0.697	100%	0.065	82%	0.072	81%	
Southern Catchment	6	0.571	0.465	100%	0.060	82%	0.047	100%	
eatermont	7	0.651	0.527	100%	0.277	92%	0.079	100%	
	Total	3.232	2.023	100%	0.637	87%	0.294	51%	

#### 5.3.2 Developed MUSIC Model

A MUSIC model was developed to incorporate a series of treatment devices including the following:

- Enviropod;
- Rainwater Tanks;
- HumeGard; and
- Humeceptor.

Please find Figure 9 for the proposed MUSIC layout.

#### The Avenue ainwat 3) Cat 1 Roof -184 ha [Roof]I - 0.207 ha [Sealedroad] Cat 1 1 UK 0.367 ha [Mixed] at 2 I Mived Bypass / Nodelt 2 Sea Post-F Φ Cat 3 0 Mixed] Cat 4 Roof 0.38 ha :at 0.28 ha [Ro Raii ater E. C at 5 Seal nviropod - 4 pitsed Road 0 Cat 3 Roof Bypass ou na Cat 5 R 1 er Tank B4 water Tank W3 Envir 6 HG30/ eptor STC18 Hur egard HG18 650 centor STC18 Hum Southern Catchment Annie Street unctio Junction

#### Figure 9: MUSIC Layout

#### 5.3.2.1 Enviropods®

All surface inlet pits within the project site have been designed to be provided with pit inserts including oil absorbent media. The pit inserts will be beneath the stormwater pit grates and will collect gross pollutants, sediments, oils and grease.

### 5.3.2.2 Rainwater Tanks

Rainwater tanks have been utilised as a means of water reuse within the project site. Stormwater that discharges directly from roof areas is generally considered as 'clean' water, with the roof water from the buildings modelled to discharge directly to a rainwater harvesting tank. These tanks are to store water for re-use associated with the proposed deployment such as toilet flush. Rainwater tanks have been sized by the project Hydraulic Engineer as indicated in Section 4.3.3.1.

## 5.3.2.3 HumeGard®

For primary treatment of the stormwater runoff, a HumeGard® Gross Pollutant Trap is to be provided. The HumeGard is a pollution control device specifically designed to remove gross pollutants and coarse sediments in residential and commercial developments. The MUSIC node from Hume's was used for this model.

## 5.3.2.4 HumeCeptor®

For secondary treatment of the stormwater runoff, a HumeCeptor® Gross Pollutant Trap is to be provided. The HumeCeptor is a pollution control device specifically designed to remove hydrocarbons and fine suspended solids from stormwater runoff generated in residential and commercial developments. The MUSIC node from Hume's was used for this model.

## 5.4 MUSIC Results

Results of the MUSIC analysis indicate that by including the nominated treatment devices as described in Section 5.3.2, the water quality improvement objectives for total suspended solids and total nitrogen set out in Council's DCP are achieved for the site but not total phosphorus and gross pollutants. Table 15 displays the results of the MUSIC model.

#### Table 15: MUSIC Model Results Total Suspended Solids (kg/yr) Total Phosphorous (kg/yr)

	Total Suspended Solids (kg/yr)	Total Phosphorous (kg/yr)	Total Nitrogen (kg/yr)	Gross Pollutants (kg/yr)
Reductions	90%	63%	60%	94%
Objectives	85%	65%	45%	90%

## 6 Desktop Flood Study

Based on email correspondence between The City of Newcastle Council and Ghazal Hosseini from Mott MacDonald dated on 1<sup>st</sup> May 2017, it is understood that the Flood Information Certificate provided by Council has the relating information of the proposed lots. Therefore, the flood modelling is not required for lodgement of the proposed development application.

## 6.1 Flood management policy and Guidelines

The flood assessment of the proposed development has been completed to comply with the following guideline and previous flood study:

- Newcastle City-wide Floodplain Risk Management Study and Plan, June 2012;
- Throsby, Cottage and CBD Flood Study, August 2008;

## 6.2 Data

The flood assessment of the subject site has been done based on following present information:

- Site Survey provided by Monteath & Powys dated on 3<sup>rd</sup> May 2017;
- Proposed Masterplan architectural layout and Woolstore 1 architectural layout provided by Tonkin Zulaikha Greer Architects and Fairweather Architecture dated on 28<sup>th</sup> March 2017 and 5<sup>th</sup> June 2017 respectively; and
- Flood Information Certificate provided by Council dated 24<sup>th</sup> August 2016.

#### 6.3 Flood Evaluation

Based on Council's Flood Information Certificate (FIC), which is based on the Newcastle Citywide Floodplain Risk Management Plan and the Newcastle Development Control Plan, the subject site is not affected by a floodway. However, the FIC indicates that the entire subject site is affected by a flood storage area. This limits ground-level development (not on stilts/piers) to 20% of the total site area.

#### 6.3.1 Flood Storage Area

Estimated flood storage provided for this site is provided in Table 16.

#### Table 16. Flood Storage Area Calculated

		Maximum allowable area (m²)	Total Area (m <sup>2</sup> )
Total Site Area	31,277 m <sup>2</sup>		31,277
Ground-Level Site Coverage	20%	6,255	5,056
Minimum Flood Storage Area	80%		26,221

As shown in Table 16, the proposed ground-level site coverage does not exceed the allowable area provided by Council.

#### 6.3.2 Minimum Floor Level

The estimated 1% Annual Exceedance Probability event level, equivalent to the "Defined Flood Level" in the *Building Code of Australia,* is 2.2m. The minimum floor level for the new development provided in the FIC is **2.5m** AHD.

The highest Property Hazard Category for the development site is P2 for the development site. Based on this category, the flood risk is too great to permit a basement car park on the site. However, parked or moving heavy vehicles are permitted. The proposed carpark floor level is 2.5m AHD, 0.3 m above 1% AEP events.

#### 6.3.3 Onsite Flood Refuge

The development site falls under Life Hazard Category L4. The Newcastle DCP states that an Onsite Flood Refuge area is required for category L4. The minimum Onsite Refuge level is to be the level of the Probably Maximum Flood (PMF). The PMF level is 3.4 AHD for the development site. Based on Council's DCP, the proposed development includes buildings greater than two stories high and the upper floor area can be used as an onsite refuge area. However, the structure type must be able to withstand the hydraulic loading due to flooding at the PMF level.

## Appendices

- A. DRAINS Inputs
- B. DRAINS Results

24 26

# **A. DRAINS Inputs**

ame	Туре	Family		Volume	Pressure Change Coeff. Ku	Surface Elev (m)	Max Pond Depth (m)		Blocking Factor		x y	Bolt-do		Part Full Shock Los	Inflow s Hydrogra	Pit aph
	Sag	NSW RTA S		11.619	5.8		0.15				-6332260	-682935 No	4747		No	Net
	Sag	NSW RTA S		12.857	2		0.15				-6332267	-682942 No	4749		No	Ne
	Sag	NSW RTA S		9.878	0.3		0.15			0	-6332273	-682942 No	4750		No	Ne
	Sag	NSW RTA S		11.186	0.3	1.49	0.15			0	-6332279	-682935 No	4851		No	Ne
	Sag	NSW RTA S		7.887	0.3		0.15			0	-6332279	-682930 No	4855		No	Ne
	Sag	NSW RTA S		17.556	0.5	1.34	0.15			0	-6332324	-682930 No	4783		No	Ne
A - H0	GOnGrade	Junction Pi	Junction Pit	t or Manho	1.5	1.64			0	0	-6332335	-682925 Yes	21945728	1 x Ku	No	Ne
A - ST	۲(OnGrade	Junction Pi	Junction Pit	t or Manho	1.5	1.38			0	0	-6332347	-682925 Yes	21945729	1 x Ku	No	Ne
	OnGrade	NSW RTA S	SB Pit		4	1.11			0	0	-6332358	-682930 No	4781	1 x Ku	No	Ne
	OnGrade	NSW RTA S	SB Pit		1.5	1.11			0	0	-6332358	-682935 No	4782	1 x Ku	No	Ne
1B	Node					0.84			0		-6332364	-682944	4798		No	
	Sag	NSW Dept.	RM7	0.729	0.5	1.17	0.15		0	0	-6332358	-682982 No	4789	1 x Ku	No	Ne
1A	Node					0.98			0		-6332363	-682982	4800		No	
	Sag	NSW RTA S	SB Pit	18.756	3.4	1.59	0.15		0	0	-6332266	-682923 No	4793	L x Ku	No	Ne
	Sag	NSW RTA S	SB Pit	15.342	0.3	1.59	0.15		0	0	-6332272	-682923 No	4753		No	Ne
f 5A	Node					2.5			0		-6332357	-682984	5275		No	
	OnGrade	NSW Dept.	RM7		1.4	1.23			0	0	-6332357	-682985 No	4788	1 x Ku	No	Ne
1C	Node					1.01			0	-	-6332358	-682990	4942		No	
f 5B	Node					2.5			0		-6332307	-682984	5276		No	
		NSW Dept.	DM7		2.1					0	-6332307	-682985 No	4790	I v Ku	No	Ne
f 1C	Node	NSW Dept.			2.1	2.5			0	U	-6332219	-682942	5321	LXKU	No	INC
I IC			CD Dit	28,731			0.15			0						
	Sag	NSW RTA S			1.5		0.15				-6332219	-682936 No	4746		No	Ne
IOA		Junction Pi			1.5						-6332205	-682940 Yes	39258670		No	Ne
18	OnGrade	Junction Pi			1.5						-6332193	-682940 Yes	39258671		No	Ne
	Sag	NSW RTA S		24.106	1.5		0.15		-		-6332180	-682936 No	4745		No	Ne
		NSW RTA S	SB Pit		1				-	0	-6332152	-682937 No	4748	L x Ku	No	Ne
2	Node					1.08			0		-6332148	-682930	4811		No	
f 1A	Node					2.5			0		-6332155	-682942	5326		No	
	OnGrade	NSW Dept.	RM7		2.5	1.4			0	0	-6332152	-682942 No	4893	1 x Ku	No	Ne
f 2C	Node					2.5			0		-6332220	-682873	5393		No	
	Sag	NSW RTA S	SB Pit	34.006	2		0.15			0	-6332220	-682876 No	4761	L x Ku	No	Ne
	Sag	NSW RTA S		18.055	1.3		0.15			ō	-6332195	-682876 No	4760		No	Ne
E - H4	G OnGrade	Junction Pi			1.5					o	-6332169	-682875 Yes	28128576		No	Ne
	COnGrade	Junction Pi			1.5					0	-6332166	-682875 Yes	28128577		No	Ne
1 - 21	OnGrade	NSW RTA S		Con renation	1.5					0	-6332166	-682875 Yes -682876 No	28128577		NO NO	Ne
				tor Maak												
-	OnGrade	Junction Pi	Junction Pil	ur ivlanno	0.5					0	-6332148	-682873 Yes	4767	LXKU	No	Ne
3	Node					1.02			0		-6332148	-682859	4817		No	
f 2B	Node					2.5			0		-6332195	-682873	5394		No	
f 2A	Node					2.5			0		-6332154	-682873	5395		No	
f 3D	Node					2.5			0		-6332225	-682818	5455		No	
	Sag	NSW RTA S	SB Pit	10.363	2.6	2.31	0.15		0		-6332225	-682821 No	4762	1 x Ku	No	Ne
	Sag	NSW RTA S	SB Pit	10.494	1.3	2.31	0.15		0	0	-6332205	-682821 No	4763	1 x Ku	No	Ne
	Sag	NSW RTA S	SB Pit	13.095	1.1	2.31	0.15		0	0	-6332185	-682821 No	4764	L x Ku	No	Ne
G - H	GOnGrade	Junction Pi	Junction Pit	t or Manho	1.5	2.38			0	0	-6332174	-682820 Yes	28128650	L x Ku	No	Ne
	T(OnGrade	Junction Pi			1.5	1.89			0	0	-6332159	-682820 Yes	28128651	1 x Ku	No	Ne
	OnGrade	NSW RTA S			1.2						-6332151	-682821 No	4766		No	Ne
		Junction Pi		t or Manho	2.5						-6332148	-682819 Yes	4769		No	Ne
nmy		Junction Pi			2.5	1.1					-6332148	-682807 Yes	6373		No	Ne
		JUNCTION PI	JUNCTION PI		2				0	U				LXKU		INC
4 f 3C	Node Node					0.94			0		-6332146 -6332205	-682807 -682818	4820 5456		No No	
									-							
f 3B	Node					2.5			0		-6332185	-682818	5457		No	
f 3A	Node					2.5			0		-6332151	-682818	5461		No	
f 3E	Node					2.5			0		-6332151	-682790	5608		No	
	OnGrade	NSW RTA S	SB Pit		1.8	1.29				0	-6332150	-682783 No	4772	1 x Ku	No	Ne
	OnGrade	Junction Pi	Junction Pit	t or Manho	0.5	1.1			0	0	-6332148	-682793 Yes	4771	1 x Ku	No	Ne
f 3F	Node					2.5			0		-6332185	-682789	5615		No	
	Sag	NSW RTA S	SB Pit	9.791	1	1.34	0.15		0	0	-6332185	-682783 No	4773	1 x Ku	No	Ne
f 3G	Node					2.5			0		-6332220	-682790	5619		No	
	Sag	NSW RTA S	SB Pit	12.4	1	1.39	0.15		0	0	-6332220	-682783 No	4774	1 x Ku	No	Ne
f 5C	Node					2.5			0		-6332358	-682943	5936		No	
f 5D	Node					2.5			0		-6332324	-682943	5937		No	
	Sag	NSW RTA S	SB Pit	22.723	-0.7	1.34	0.15			0	-6332324	-682935 No	4784	I x Ku	No	Ne
f 5E	Node			22.123	-0.7	2.5	0.15		0	5	-6332324	-682935 NO	5938		NO	ive
						2.5										
f 5F	Node								0		-6332278	-682943	5939		No	
	PrNode					1.01			0		-6332373	-682985	1301572		No	
	PiNode					0.98			0		-6332372	-682982	1514766		No	
	PrNode					0.84			0		-6332372	-682943	1641602		No	
	tlNode					0.83			0		-6332389	-682945	1641616		No	
	tlNode					0.82			0		-6332397	-682945	1641618		No	
	or Node					0.83			0		-6332387	-682932	1879422		No	
ost No	or Node					0.82			0		-6332397	-682932	1879423		No	
at 2 Pr	eNode					1.08			0		-6332131	-682930	4310294		No	
	eNode					1.02			0		-6332132	-682859	4310311		No	
	eNode					0.94			0		-6332134	-682807	4310327		No	
	tiNode					0.8			0		-6332129	-682807	4310345		No	
	tiNode					0.79			0		-6332120	-682807	4310347		No	
	a Node					1			0		-6332276	-682994	4310350		No	
	a Node					1			0		-6332270	-682994	4310363		No	
	tiNode					0.8			0		-6332131	-682798	4635470		No	
	tiNode					0.79			0		-6332122	-682799	4635482		No	
	Sag	NSW Dept.	RM7	5	1.5					n	-6332324	-682896 No	14702516	L x Ku	No	Ne
	Sag	NSW RTA S		8.016	1.5						-6332256	-682825 No	26893867		No	Ne
					4		0.15								NO	Ne
	Sag	NSW RTA S	30 PIL	5.143	4		0.15			U	-6332256	-682821 No	26893873	LXKU		Ne
ltex	Node					1.42			0		-6332272	-682814	28957917		No	
f1B	Node					2.5			0		-6332180	-682943	38766330		No	
	Node					2.5			0		-6332156	-682984	40732630		No	
of 2D	Node					2.5			0		-6332224	-682832	40732668		No	
	Sag	NSW RTA S	SB Pit	10.363	2.6	2.31	0.15		0	0	-6332225	-682825 No	26893878	1 x Ku	No	Ne
	Node					2.5			0		-6332204	-682833	40732670		No	
	Sag	NSW RTA S	SB Pit	10.494	1.3	2.31	0.15			0	-6332205	-682825 No	26893882	L x Ku	No	Ne
	Node			10.404	1.3	2.51	0.15		0	5	-6332203	-682832	40732672		No	140
DOT 2F		NSM DTA C	CB Dit	13.095	1.1		0.15		-	c	-6332185	-682832 -682825 No	26893936	I v Ku	NO NO	Ne
	Sag	NSW RTA S	JOFIL	13.095	1.1		0.15			U				L X KU		NE
	6 Node					2.5			0		-6332154	-682832	40732674		No	
1	OnGrade	NSW RTA S	SB Pit		1.2	1.31			0	0	-6332151	-682826 No	26893891	L x Ku	No	Ne
	ON BASIN DE		Not !!- '	0+!-+ ~	v	Dia()	Contro 21	Dit 7	Die T				Cr+ ?'	Prost /	Tid	
				Outlet Type	ĸ	Dia(mm)	Centre RL	Pit Famil	v Pit Type		x )	HED	Crest RL	rest Len	gtid	
ne	Elev	Surf. Area							/ . // .							
	0.585	2		Culvert	0.5				, ,,,,			-682923 No			313975	53
e		2							, ,,,,						313975	53

SUB-CAT	CHMENT DE	TAILS																			
Name	Pit or	Total	Paved	Grass	Supp	Paved	Grass	Supp	Paved	Grass	Supp	Paved	Grass	Supp	Paved	Grass	Supp	Lag Time	Gutter	Gutter	Gutter Rainfall
	Node	Area	Area	Area	Area	Time	Time	Time	Length	Length	Length	Slope(%)		Slope	Rough	Rough	Rough	or Factor		Slope	FlowFactor Multiplier
		(ha) 0.023	%	%	%	(min)	(min)	(min) 10	(m) 0	(m)	(m)	%	%	%					(m)	%	
Cat L4 Cat L3	L4 L3	0.023		92 84	8 16	0	5 5	10	0												
Cat L2	L2	0.023		93	7	0	5	10	0												
Cat L1	L1	0.022		90	10	0	5	10	0												
Cat A5	A5	0.015		86	14	0	5	10	0												
Cat A4	A4	0.035		86	14	0	5	10	0												
	asi A3 Basin	0.19		13	87	0	5	10	0												
Cat A2 Cat A1	A2 A1	0.015		81 75	19 25	0	5 5	10 10	0												
Cat B1	B1	0.021		0	100	0	5	10	0												
Cat M1	M1	0.031		94	6	0	5	10	0												
Cat A6	A6	0.025	5	91	9	0	5	10	0												
	5/Roof 5A	0.101		100	0	0	5	10	0												
Cat C1	C1	0.008		27	73	0	5	10	0												
Cat Roof Cat C2	5ERoof 5B C2	0.061		100 23	0 77	0	5 5	10 10	0												
	1(Roof 1C	0.005		100	0	0	5	10	0												
Cat D3	D3	0.057		74	26	0	5	10	0												
Cat D2	D2	0.048		98	2	0	5	10	0												
Cat D1	D1	0.017		46	54	0	5	10	0												
	1/Roof 1A	0.113		100	0	0	5	10	0												
Cat E1	E1	0.013			100	0	5	10	0												
Cat Roor Cat F4	2(Roof 2C F4	0.20 0.035		100 99	0	0	5 5	10 100	0												
Cat F4	F4	0.035		99	1	0	5.	10	0												
Cat F2	F2	0.03		72	28	0	5	10	0												
Cat Roof	2ERoof 2B	0.132	5	100	0	0	5	10	0												
	2/Roof 2A	0.128		100	0	0	5	10	0												
	3I Roof 3D	0.049		100	0	0	5	10	0												
Cat G5	G5 G4	0.0		100	0	0	5	10	0												
Cat G4 Cat G3	G4 G3	0.010		100 100	0	0	5 5	10 10	0												
Cat G2	G2	0.010		100	0	0	5	10	0												
	3(Roof 3C	0.027		100	0	0	5	10	0												
Cat Roof	3ERoof 3B	0.027	4	100	0	0	5	10	0												
	3/Roof 3A	0.032		100	0	0	5	10	0												
	3ERoof 3E	0.029		100	0	0	5	10	0												
Cat H2	H2 3FRoof 3F	0.015		72 100	28 0	0	5 5	10 10	0												
Cat Roor		0.055		84	16	0	5	10	0												
Cat Roof	3(Roof 3G	0.023		100	0	0	5	10	0												
Cat H4		0.032		88	12	0	5	10	0												
	5(Roof 5C	0.041		100	0	0	5	10	0												
	5I Roof 5D	0.095		100	0	0	5	10	0												
	J1	0.045		93	7	0	5	10	0												
	5I Roof 5E 5I Roof 5F	0.017		100 100	0	0 0	5 5	10 10	0												
	re N Cat 1C F			97	3	0	5	10	0												
	re N Cat 1A F			17	83	0	5	10	0												
Cat 1B Pr	e N Cat 1B F	0.328	6	100	0	0	5	10	0												
	N Cat 2 Pr			99	1	0	5	10	0												
	N Cat 3 Pr			100	0	0	5	10	0												
	N Cat 4 Pr			90 97	10 3	0	5	10 10	0												
	ss N Cat Byp ss N Cat Byp			97 84	3 16	0	5 5	10	0												
Cat Bypa Cat K1	K1	0.033		0	100	0	5	10	0												
Cat G7	G7	0.118		100	0	0	5	10	0												
Cat G6	G6	0.078		100	0	0	5	10	0												
	1ERoof 1B	0.168		100	0	0	5	10	0												
	1(N Roof 1D			100	0	0	5	10	0												
	2IN Roof 2D			100	0	0	5	10	0												
Cat G5A	G5A 2EN Roof 2E	0.010 0.043		100 100	0 0	0 0	5 5	10 10	0												
Cat Roor Cat G4A		0.043		100	0	0	5	10	0												
	2FN Roof 2F	0.010		100	0	0	5	10	0												
Cat G3A		0.010	19	100	0	0	5	10	0												
	2(N Roof 2G			100	0	0	5	10	0												
Cat G2A	G2A	0.013	3	100	0	0	5	10	0												

IPE DETA lame	From					Slope	Туре	Dia	I.D.		ough	Pipe Is	No. Pipes	Chg From At Chg	Chg	RI	Chg	RL (m)	etc
14	14	L3	(m) 10.452	(m) 1.109	(m) 1.057	(%) 0 '	o Concrete,	(mm)	(mm) 300	300	0.013	New	1	L L4	(m) 0	(m)	(m)	(m)	(m)
L3	L3	L2	4.8	1.037	1.013		o Concrete,		300	300	0.013			1 L3	0				
2	L2	L1	9.347	0.993	0.946		6 Concrete.		300	300	0.013			L L2	0				
1	11	A5	4.803	0.926	0.902		6 Concrete,		300	300	0.013			1	0				
45	A5	A4	44.099	0.882	0.662		Box culver					Existing		L A5	0				
14	A4	A3 Basin	7.379	0.642			Box culver					Existing		2 A4	0				
A3 Basin	A3 Basin	Line A - HG		0.585	0.457		Concrete,		300	300		NewFixed		A3 Basin	0				
HG18	Line A - HO	G Line A - ST		0.437	0.387		Concrete,		300	300	0.013		1	L Line A - HG	0				
ne A - PS	Line A - ST		5.08	0.367	0.342		Oncrete,		300	300	0.013	New		Line A - ST(	0				
42	A2	A1	4.8	0.322	0.298		Box culver		x 0.3H			Existing		A2	0				
A1	A1	Cat 1B	9.676	0.278	0.23		Concrete,		300	300	0.013		2	2 A1	0				
B1	B1	Cat 1A	3.985	0.445			6 Concrete,		300	300	0.013			B1	0				
M1	M1	A6	4.8	0.983	0.959		6 Concrete,		300	300	0.013			M1	0				
A6	A6	A5	7.426	0.939	0.902		6 Concrete,		300	300	0.013	New		A6	0				
	Roof 5A	C1	1	0.643	0.633		Concrete,		300	300	0.013			Roof 5A	0				
C1	C1	Cat 1C	4.639	0.613	0.59		6 Concrete,		300	300	0.013			2 C1	0				
	Roof 5B	C2	4.055	0.904	0.894		Concrete,		300	300	0.013			L Roof 5B	0				
C2	C2	C1	48.245	0.874			6 Concrete,		300	300	0.013			L C2	0				
		D3	40.243	0.814	0.033				300	300	0.013				0				
ROOT 1C	Roof 1C D3	HG30A		0.814			Concrete,			300				PROOF 1C	0				
			3.769		0.755		Box culver					NewFixed							
HG30A	HG30A	STC18	7.195	0.755	0.71		Box culver					NewFixed		HG30A	0				
STC	STC18	D2	24.731	0.71	0.586		Box culver					NewFixed		STC18	-				
D2	D2	D1	27.486	0.566	0.429		Box culver					NewFixed		L D2	0				
D1	D1	Cat 2	7.772	0.409	0.37		Box culver				0.012			2 D1	0				
	Roof 1A	E1	1	0.482	0.472		Concrete,		300	300	0.013			Roof 1A	0				
E1	E1	D1	4.51	0.452			Box culver					Existing		L E1	0				
	Roof 2C	F4	1	0.8	0.79		Concrete,		300	300	0.013			2 Roof 2C	0				
4	F4	F3	24.1	0.77	0.65		Box culver					NewFixed		F4	0				
3	F3	Line F - HG	24.2	0.63	0.509		5 Box culver					Existing		L F3	0				
ne F - PH	KLine F - HG	6 Line F - STO	5	0.509	0.484	0.5	5 Box culver	t0.9W	x 0.3H		0.012	NewFixed	1	L Line F - HG	0				
	TLine F - ST	C F2	9	0.465	0.42		6 Box culver					NewFixed		L Line F - STC	0				
F2	F2	F1	4.52	0.398	0.375	0.5	Box culver	t0.9W	x 0.3H		0.012	NewFixed	2	2 F2	0				
F1	F1	Cat 3	14.966	0.355	0.28	0.5	6 Box culver	t0.9W	x 0.3H		0.012	New	2	2 F1	0				
Roof 2B	Roof 2B	F3	1	0.66	0.65	1	Concrete,	r	300	300	0.013	New	1	Roof 2B	0				
Roof 2A	Roof 2A	F2	1	0.428	0.418	1	Concrete,	r	300	300	0.013	New	1	Roof 2A	0				
	Roof 3D	G5	1	0.861			Concrete,		300	300	0.013	New		Roof 3D	0				
G5	G5	G4	19.1	0.831	0.735	0.5	Box culver	11.8W	x 0.3H			Existing		2 G5	0				
G4	G4	G3	19.1	0.715	0.619	0.5	6 Box culver	11.8W	x 0.3H		0.012	Existing	2	2 G4	0				
G3	G3	Line G - HG		0.599	0.551	0.5	Box culver	11.2W	x 0.3H		0.012	Existing	1	G3	0				
ine G - PH	Line G - H	G Line G - ST		0.55	0.499		Box culver					Existing	1	L Line G - HG	0				
	(Line G - ST		8.55	0.483	0.44		Box culver					Existing		L Line G - ST(	0				
G2	G2	G1	4.656	0.417			Box culver					Existing		G2	0				
G1	G1	Dummy	10.858	0.374	0.32		Box culver					Existing		2 G1	0				
	Dummy	Cat 4	10.050	0.3	0.3		) Box culver					NewFixed		2 Dummy	0				
	Roof 3C	G4	10	0.745	0.735		Concrete,		300	300	0.012			Roof 3C	0				
	Roof 3B	G3	1	0.629			Concrete,		300	300	0.013			Roof 3B	0				
	Roof 3A	G2	1	0.447	0.437		Concrete,		300	300	0.013			Roof 3A	0				
	Roof 3E	H2	1	0.447	0.469		L Concrete,		300	300	0.013			Roof 3E	0				
H2	H2	H1	9.426	0.475	0.402		Box culver			500		NewFixed		L H2	0				
H1	H2 H1	Dummy	12.497	0.382	0.402		6 Box culver					NewFixed		L H1	0				
	Roof 3F	H3	12.497	0.382	0.32		Concrete,		300	300	0.012			Roof 3F	0				
H3										500									
	H3	H2 H4	33.36	0.636	0.469		Box culver			202		NewFixed		L H3	0				
	Roof 3G		1	0.856	0.846		Concrete,		300	300	0.013			Roof 3G					
14	H4	НЗ	34.1	0.826	0.656		Concrete,		300	300	0.013			2 H4	0				
	Roof 5C	A1	1	0.308	0.298		Concrete,		300	300	0.013			Roof 5C	0				
	Roof 5D	J1	1	0.634	0.624		Concrete,		300	300	0.013			L Roof 5D	0				
1	J1	A4	4.8	0.686			Box culver					Existing		2 J1	0				
	Roof 5E	L1	2	0.956			Concrete,		300	300	0.013			L Roof 5E	0				
	Roof 5F	L2	2	1.015	1.013		Concrete,		300	300	0.013			L Roof 5F	0				
(1	К1	A3 Basin	23.883	0.724	0.605		6 Box culver					Existing		L K1	0				
G7	G7	G6	2.7	1.018	1.004		2 Concrete,		225	225	0.013			L G7	0				
G6	G6	G5	26.6	0.984			6 Concrete,		225	225	0.013			3 G6	0				
	Roof 1B	D2	1	0.596			Concrete,		300	300	0.013			Roof 1B	0				
	N Roof 1D		1	0.482			Concrete,		300	300	0.013			N Roof 1D	0				
Roof 2D	N Roof 2D	G5A	2	0.904	0.884	1	Concrete,	r	300	300	0.013	New	2	N Roof 2D	0				
35A	G5A	G5	2.7	0.864	0.851		Concrete,		300	300	0.013	New	2	2 G5A	0				
	N Roof 2E	G4A	1	0.778	0.768		Concrete,	r	300	300	0.013	New	2	N Roof 2E	0				
54A	G4A	G4	2.7	0.748	0.735	0.48	Concrete,	ι	300	300	0.013	New	2	2 G4A	0				
Roof 2F		G3A	1	0.662	0.652		Concrete,		300	300	0.013			N Roof 2F	0				
G3A	G3A	G3	2.7	0.632	0.619		Concrete.		300	300	0.013			2 G3A	0				
	N Roof 2G		1	0.481	0.471		Concrete,		300	300	0.013			N Roof 2G	0				
G2A	G2A	G2	2.7	0.451			Concrete,		300	300	0.013			2 G2A	0				
		~~	2.7	5.451	5.457	0.5	. sonarete,	-		500	0.015		4		-				
FTAILS	f SERVICES	CROSSING P	IPES																
pe	Chg (m)		Height of S	Chg (m)	Bottom Elev (m)	Height of (m)	S Chg (m)	Botto Elev (r		nt of Set m) et									
	DETAILS																		
ame	From	То	Type	Length	U/S IL	D/S IL	Slope	Base \	Vidtł L.B. S	lone R	B. Slope	Manning	Depth	Roofed					

		ETAILS													
Name	From	То	Travel		Spill	Crest		Weir	Cross		SafeDepth		Bed	D/S Area	id
			Time		Level	Leng	th	Coeff.	C Section		Minor Stor		Slope	Contributing	
			(min)		(m)	(m)				(m)	(m)	(sq.m/sec)		%	6000
OF L4	L4	L3		0.1					4 m wide p						6338
OF L3	L3	L2		0.1					Overflow a						3990695
OF L2	L2	L1		0.1					7.5 m road						3990697
OF L1	L1	J1		0.1					4 m wide j						6335
OF A5	A5	A4		0.5					7.5 m road						3990719
OF A4	A4	A2		0.3					7.5 m road						3990724
	sirA3 Basin	A4		0.1	1	.56	20	) :	1.74 Overflow a						3990734
OF A2	A2	Cat 1B		0.1					4 m wide p				-		6328
OF A1	A1	Cat 1B		0.1					4 m wide j						6329
OF Cat 1B		N Post Nor		0.1					7.5 m road						1879414
OF B1 - O		Cat 1A		0.1					4 m wide j						5253
OF Cat 1A		N Post Nor		0.1					7.5 m road						1879416
OF M1 - A		A6		0.1					DD Wool F						6322
OF A6	A6	A5		0.1					7.5 m road						3990700
OF C1 - O		Cat 1C		0.1					4 m wide j						5388
OF Cat 10		N Post Nor		0.1					7.5 m road						1879419
OF C2 - C		Cat 1C		0.6					4 m wide j						4944
OF D3 - D		D2		0.6					DD Lanew						5060
OF D2 - D		D1		0.4					DD Lanew						5062
OF D1 - O		Cat 2		0.1					4 m wide j						5379
OF Cat 2 F		N Cat Sout	1	0.1					7.5 m road	± 0.3	0.15	0.36			4635466
OF E1 - D		D1		0.2					4 m wide j	o 0.3	0.15	0.4	0.59		5386
OF F4 - F3	F4	F3		0.2					4 m wide j	o 0.3	0.15	0.4	1	1 50	5124
OF F3	F3	F2		0.7					DD Lanew	a 0.1	0.05	0.36	1		28128623
OF F2 - O	ut F2	Cat 3		0.1					4 m wide j	o 0.3	0.15	0.4	1.17	7 100	5392
OF Cat 3 F	Cat 3	N Cat Sout	1	0.1					7.5 m road	± 0.3	0.15	0.36	1	1 0	4635469
OF G5 - G	4 G5	G4		0.3					DD Lanew	a 0.1	0.05	0.36	i 1	1 50	5240
OF G4 - G	3 G4	G3		0.3					DD Lanew	a 0.1	0.05	0.36	1	1 50	5241
OF G3 - G	2 G3	G2		0.5					DD Lanew	a 0.1	0.05	0.36	i 1	1 30	5242
OF G2 - O	u G2	Cat 4		0.1					4 m wide p	o 0.3	0.15	0.4	2.59	9 100	5468
OF N Cat	4 Cat 4	N Cat Sout	1	0.1					7.5 m road	± 0.3	0.15	0.36	i 1	1 0	4635476
OF H2 - O	u H2	Cat 4		0.2					4 m wide p	o 0.3	0.15	0.4	1.57	7 100	5560
OF H3 - H	2 H3	H2		0.5					DD Wool F	R 0.1	0.05	0.36	1	1 50	5614
OF H4 - H	3 H4	Н3		0.5					DD Wool F	R 0.1	0.05	0.36	1	1 50	5626
OF J1	J1	A1		0.3					7.5 m road	± 0.3	0.15	0.36	1.2	2 0	3990742
OF Cat 1C	FN Cat 1C	N Pre Nort	1	0.1					7.5 m road	± 0.3	0.15	0.36	1	1 0	1641627
OF Cat 1A	IN Cat 1A	N Pre Nort	i i	0.1					7.5 m road	± 0.3	0.15	0.36	; 1	1 0	1641623
OF Cat 1B	FN Cat 1B	N Pre Nort	1	0.1					7.5 m road	± 0.3	0.15	0.36	1	1 0	1641622
OF Pre No	or N Pre Nor	t N Pre Nort	1	0.1					7.5 m road	± 0.3	0.15	0.36	1	1 0	1641631
OF Post N	o N Post No	r N Post Nor		0.1					7.5 m road	± 0.3	0.15	0.36	; 1	1 0	1879425
OF N Cat	2 N Cat 2 Pr	e N Cat Sout	1	0.1					7.5 m road	t 0.3	0.15	0.36	1	1 0	4635457
		e N Cat Sout		0.1					7.5 m road		0.15	0.36	; 1	1 0	4635454
OF N Cat	4 N Cat 4 Pr	e N Cat Sout	1	0.1					7.5 m road		0.15	0.36	. 1	1 0	4635446
		t N Cat Sout		0.1					7.5 m road						4635447
		a N Pre Nort		0.1					7.5 m road		0.15			1 0	4310353
		a N Post Nor		0.1					7.5 m road						4310372
		t N Cat Sout		0.1					7.5 m road						4635480
DF K1	K1	A3 Basin		0.2					4 m wide i					1 100	14702522
OF G7	G7	G6		0.1					7.5 m road						26894193
OF G6	G6	N Caltex		0.1					7.5 m road						26894194
OF G5A	G5A	G4A		0.1					7.5 m road						26893940
OF G4A	G4A	G3A		0.2					7.5 m road						26893940
OF G4A	G3A	G2A		0.2					DD Lanew						26893942
		UZM		0.0										. 0	

PIPE COVE	R DETAILS			
Name		Dia (mm)	Safe Cover	Cover (m)
PL4	Concrete,		0.6	0.17
PL3	Concrete,		0.6	0.2
PL2	Concrete,		0.45	0.21
PL1 PA5	Concrete,		0.6	0.23
PA5 PA4	Box culver		0.6 0.6	0.11
	Box culver Concrete, i	-	0.6	-0.52
PHG18	Concrete,		0.45	0.66
Line A - PS	Concrete,		0.45	0.44
PA2	Box culver		0.6	0.29
PA1	Concrete,		0.45	0.28
PB1	Concrete,		0.45	0.22
PM1	Concrete,		0.6	0.28
PA6 PRoof 5A	Concrete, i Concrete, i		0.45	0.26 0.27
PC1	Concrete, I		0.45	0.27
PRoof 5B	Concrete,		0.45	0.13
PC2	Concrete,		0.45	0.15
PRoof 1C	Concrete,		0.45	0.28
PD3	Box culver		0.6	0.14
PHG30A	Box culver		0.6	0.27
PSTC	Box culver		0.6	0.12
PD2 PD1	Box culver Box culver		0.6 0.6	0.14 0.21
PRoof 1A	Concrete,		0.45	0.21
PF1	Box culver		0.6	0.38
PRoof 2C	Concrete,		0.45	0.29
PF4	Box culver	0	0.6	0.14
PF3	Box culver		0.6	0.24
	(Box culver		0.6	0.46
Line F - PS PF2	Box culver Box culver		0.6 0.6	0.29 0.29
PF2 PF1	Box culver		0.6	0.29
PRoof 2B			0.45	0.39
PRoof 2A			0.45	0.46
PRoof 3D			0.45	1.13
PG5	Box culver		0.6	0.98
PG4 PG3	Box culver		0.6	1.09
	Box culver Box culver		0.6	1.21
Line G - ST	(Box culver	0	0.6	0.37
PG2	Box culver		0.6	0.21
PG1	Box culver		0.6	0.23
To Outlet	Box culver		0.6	0.14
PRoof 3C PRoof 3B	Concrete,		0.45	1.24
PRoof 3A	Concrete, i Concrete, i		0.45	1.36 0.54
PRoof 3E	Concrete,		0.45	0.49
PH2	Box culver		0.6	0.2
PH1	Box culver		0.6	0.22
PRoof 3F	Concrete,		0.45	0.35
PH3 PRoof 3G	Box culver Concrete, i		0.6	0.2 0.21
PROOF 3G	Concrete, I		0.45	0.21
PRoof 5C	Concrete,		0.45	0.48
PRoof 5D	Concrete,		0.45	0.39
PJ1	Box culver		0.6	0.15
PRoof 5E			0.45	0.21
PRoof 5F	Concrete,		0.45	0.23
PK1 PG7	Box culver Concrete,		0.6 0.6	-0.52 0.16
PG6	Concrete,		0.45	0.10
PRoof 1B	Concrete,		0.45	0.29
P Roof 1D	Concrete,		0.45	0.6
	Concrete,		0.45	1.09
PG5A	Concrete,		0.6	1.11
P Roof 2E PG4A	Concrete, Concrete,		0.45 0.6	1.21 1.23
PG4A P Roof 2F	Concrete,		0.6	1.23
PG3A	Concrete,		0.45	1.35
P Roof 2G	Concrete,	300	0.45	0.51
PG2A	Concrete,	300	0.6	0.53

This model has no pipes with non-return valves

## **B. DRAINS Results**

#### DRAINS results prepared from Version 2017.10

PIT / NODE DETAILS Name	Max HGL	Max Pond HGL	Max Surfac Flow Arrivi		Min Freeboard		Constraint
			(cu.m/s)	(cu.m)	(m)		
L4	1.25	1.63	0.011	0	0.36		Inlet Capacity
L3	1.21	1.59	0.012	0	0.36		Inlet Capacity
L2	1.18	1.59	0.01	0			Inlet Capacity
L1	1.14	1.51	0.011	0			Inlet Capacity
A5 A4	0.99	1.5	0.007	0			Inlet Capacity
44 Line A - HG18	1.02	1.36	0.017	0.1	0.32 0.45		Inlet Capacity
Line A - STC18	1.19 0.93		0 0		0.45		None None
A2	0.93		0.007		0.43		None
A1	0.92		0.007		0.10		None
Cat 1B	0.84		0.01		0.15	0	None
31	0.98	1.17	0.001	0	0.19	0	None
Cat 1A	0.98		0				
M1	1.12	1.61	0.015	0.1	0.47	0	Inlet Capacity
46	1.07	1.61	0.012	0	0.52	0	Inlet Capacity
Roof 5A	1.05		0.05				
C1	1.05		0.003		0.18	0	None
Cat 1C	1.01		0				
Roof 5B	1.13		0.031				
22	1.13		0.002		0.23	0	None
Roof 1C	1.26		0.12				
03	1.25	1.44	0.026	0.2			Inlet Capacity
HG30A	1.23		0		0.3		None
STC18	1.2		0		0.48		None
02	1.16	1.24	0.024	0.2			Inlet Capacity
01	1.09		0.007		0.22	0	None
Cat 2	1.08		0				
Roof 1A	1.19		0.057				
1	1.18		0.005		0.22	0	None
Roof 2C	1.25		0.101		0.46		
4	1.25	1.43	0.018	0.1			Inlet Capacity
-3 ing F HC18	1.21	1.39	0.018	0.1			Inlet Capacity
ine F - HG18	1.14		0		0.33		None
ine F - STC9	1.09 1.06		0 0.016		0.35		None
-2 -1	1.08		0.018		0.15 0.13		Inlet Capacity None
Cat 3	1.04		0.001		0.15		None
Roof 2B	1.02		0.001				
Roof 2A	1.22		0.000				
Roof 3D	1.07		0.025				
66.65	1.11	2.32	0.005	0	1.2	0	Inlet Capacity
54	1.11	2.32	0.005	0			Inlet Capacity
63	1.1	2.32	0.005	0			Inlet Capacity
ine G - HG18	1.07		0		1.31		None
ine G - STC 9	1.02		0		0.87		None
52	0.98		0.006		0.33	0	None
61	0.97		0		0.13		None
Dummy	0.96		0		0.14		None
Cat 4	0.94		0				
Roof 3C	1.11		0.014				
Roof 3B	1.1		0.014				
Roof 3A	0.98		0.016				
loof 3E	1.03		0.015				
12	1.03		0.007		0.26		None
11	0.98		0		0.12		None
loof 3F	1.07		0.027				
13	1.07	1.36		0	0.27	0	Inlet Capacity
loof 3G	1.1		0.036				
14	1.1	1.41			0.29	0	Inlet Capacity
loof 5C	0.92		0.021				
Roof 5D	1.08	<i>c</i> ==	0.047			-	Inlat Court
1 Poof FF	1.06	1.37		0.1	0.28	0	Inlet Capacity
Roof 5E	1.14		0.009				
Roof 5F	1.18	<i>c</i> ==	0.008			-	Inlat Court
(1	1.01	1.37		0.6			Inlet Capacity
67 56	1.49	1.53					Outlet System
G6 Deef 1B	1.28	1.47		0.1	0.15	0	Inlet Capacity
Roof 1B	1.16		0.084				
N Roof 1D	1.19		0.086				
N Roof 2D	1.13		0.045	-		-	lalat C
G5A	1.13	2.32		0	1.18	0	Inlet Capacity
N Roof 2E	1.11		0.022	-		-	Inlat Court
G4A	1.11	2.32	0.005	0	1.2	0	Inlet Capacity
N Roof 2F	1.11		0.022			-	lalat C
G3A	1.11	2.32		0	1.2	0	Inlet Capacity
N Roof 2G	0.98 0.98		0.026		0.33		
G2A			0.007				None

SUB-CATCHMENT DETAILS							
Name	Max	Paved	Grassed	Paved	Grassed	Supp.	Due to Storm
	Flow Q	Max Q	Max Q	Тс	Тс	Тс	
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)	
Cat L4	0.011					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat L3	0.012					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat L2	0.01					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat L1	0.011					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat A5 Cat A4	0.007 0.017					10 10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat A3 Basin	0.017					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat A2	0.007					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat A1	0.01					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat B1	0.001	. 0	0.001		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat M1	0.015	0.015	0.001		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat A6	0.012	0.012	0.001		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 5A	0.05	0.05	0			10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat C1	0.003					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 5B	0.031					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat C2	0.002					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 1C	0.12					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat D3	0.026					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat D2	0.024					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat D1 Cat Roof 1A	0.007 0.057					10 10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat E1	0.005					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 2C	0.101					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat F4	0.018					00	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat F3	0.018					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat F2	0.016					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 2B	0.066	0.066	0		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 2A	0.064	0.064	0		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 3D	0.025	0.025	0		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G5	0.005	0.005	0		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G4	0.005	0.005	0			10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G3	0.005					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G2	0.006					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 3C	0.014					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 3B	0.014					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 3A	0.016					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 3E Cat H2	0.015 0.007					10 10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 3F	0.027					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat H3	0.011					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 3G	0.036					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat H4	0.016					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 5C	0.021	0.021	0		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 5D	0.047	0.047	0		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat J1	0.022	0.021	0.001		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 5E	0.009					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 5F	0.008					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat 1C Pre	0.098					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat 1A Pre	0.003					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat 1B Pre	0.163					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat 2 Pre Cat 3 Pre	0.562 0.315					10 10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat 4 Pre	0.313					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Bypass 1 Pre	0.064					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Bypass 1 Post	0.017					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat K1	0.027					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G7	0.059					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G6	0.039	0.039	0			10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 1B	0.084	0.084	0		5	10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 1D	0.086	0.086	0			10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 2D	0.045					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G5A	0.005					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 2E	0.022					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G4A	0.005					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 2F	0.022					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat G3A	0.005					10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cat Roof 2G Cat G2A	0.026					10 10	0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 0 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Cut UZA	0.007	0.007	U		5	10	o man 20 year, 25 minutes storill, average 51.7 min/il, 2018 1

Outflow Volumes for Total Catchment (5.99 impervious + 0.47 pervious = 6.47 total ha) Storm Total Rainf Total Runo Impervious Pervious Runoff

	cu.m	cu.m (Runc	cu.m (Runc	cu.m (Runoff %	)
AR&R 20 year, 5 minutes storm, a	980.15	875.13 (89	848.78 (93	26.35 (36.9%)	
AR&R 20 year, 10 minutes storm,	1508.82	1394.50 (9	1338.93 (9	55.57 (50.5%)	
AR&R 20 year, 15 minutes storm,	1896.51	1774.69 (9	1698.37 (9	76.32 (55.2%)	
AR&R 20 year, 20 minutes storm,	2208.01	2080.25 (9	1987.18 (9	93.08 (57.8%)	
AR&R 20 year, 25 minutes storm,	2470.65	2335.41 (9	2230.67 (9	104.74 (58.2%)	
AR&R 20 year, 30 minutes storm,	2699.78	2557.94 (9	2443.08 (9	114.87 (58.4%)	
AR&R 20 year, 45 minutes storm,	3257.93	3100.99 (9	2960.57 (9	140.42 (59.1%)	
AR&R 20 year, 1 hour storm, aver	3698.03	3529.37 (9	3368.59 (9	160.77 (59.7%)	
AR&R 20 year, 1.5 hours storm, a	4323.09	4134.82 (9	3948.11 (9	186.71 (59.3%)	
AR&R 20 year, 2 hours storm, ave	4812.49	4608.11 (9	4401.86 (9	206.25 (58.8%)	

F	IPE DETAILS					
ľ	lame	Max Q	Max V	Max U/S	Max D/S	Due to Storm
			(m/s)	HGL (m)	HGL (m)	
	2L4	0.011	0.46	1.219		3 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	13	0.023	0.65	1.186		9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	L2 L1	0.04	0.94			6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	A5	0.059 0.094	1.26 0.75			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 7 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	A5 A4	0.795	0.75			3 AR&R 20 year, 20 minutes storm, average 102 mm/h, Zone 1
	A3 Basin	0.052	0.74			2 AR&R 20 year, 5 minutes storm, average 182 mm/h, Zone 1
	HG18	0.052	0.8			4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	ine A - PSTC18	0.055	0.39			1 AR&R 20 year, 45 minutes storm, average 67.2 mm/h, Zone 1
	A2	0.049	0.18			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	A1	0.087	0.61	0.899		4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	B1	0.001	0.01	0.98	0.98	8 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	M1	0.015	0.75	1.08	1.073	3 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	A6	0.027	0.98	1.062	1.027	7 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 5A	0.05	0.71			6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	C1	0.086	0.61			1 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 5B	0.031	0.54			6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	C2	0.033	0.58			6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 1C	0.12	0.85			2 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	D3 HG30A	0.143 0.144	0.53 0.53			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 3 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	STC	0.144	0.53			6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	D2	0.249	0.69			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	D1	0.404	0.37			8 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 1A	0.057	0.4			4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	'E1	0.148	0.82			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	Roof 2C	0.101	0.72	1.25	1.246	6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	F4	0.118	0.44	1.226	1.214	4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	F3	0.2	0.74	1.177	1.14	4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
L	ine F - PHG18	0.2	0.74	1.098		9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	ine F - PSTC9	0.201	0.56			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	F2	0.279	0.52			8 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	F1	0.279	0.52			2 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 2B	0.066	0.93			4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 2A Roof 3D	0.064 0.026	0.9 0.2			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 1 AR&R 20 year, 20 minutes storm, average 102 mm/h, Zone 1
	G5	0.020	0.2			7 AR&R 20 year, 25 minutes storm, average 102 min/n, 20ne 1
	G4	0.201	0.10			4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	963	0.244	0.68			6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	ine G - PHG18	0.243	0.68			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
L	ine G - STC9	0.244	0.68	0.985	0.976	6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	G2	0.302	0.28	0.971	0.97	7 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	G1	0.298	0.28	0.961	0.958	8 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
Т	o Outlet	0.406	0.38	0.945		4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 3C	0.014	0.1			7 AR&R 20 year, 15 minutes storm, average 117 mm/h, Zone 1
	Roof 3B	0.014	0.1			4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 3A	0.017	0.24			6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 3E	0.015	0.11			9 AR&R 20 year, 15 minutes storm, average 117 mm/h, Zone 1
	'H2 'H1	0.11 0.11	0.61 0.61			3 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 3F	0.028	0.01			8 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 7 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	H3	0.089	0.49	1.055		9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 3G	0.038	0.31			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	'H4	0.052	0.39	1.092		7 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	Roof 5C	0.022	0.31	0.919	0.919	9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	Roof 5D	0.062	0.88	1.079	1.064	4 AR&R 20 year, 20 minutes storm, average 102 mm/h, Zone 1
F	11	0.69	0.96	1.068	1.017	7 AR&R 20 year, 1 hour storm, average 57.2 mm/h, Zone 1
F	Roof 5E	0.009	0.2	1.137		6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 5F	0.008	0.21			9 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	K1	0.081	0.48			3 AR&R 20 year, 2 hours storm, average 37.2 mm/h, Zone 1
	G7	0.045	1.14			7 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	G6	0.076	0.64			1 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	Roof 1B	0.084	0.6			6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	P Roof 1D P Roof 2D	0.087 0.044	0.61 0.39			4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1 3 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	G5A	0.044	0.39			1 AR&R 20 year, 25 minutes storm, average 91.7 mm/n, 20ne 1
	Roof 2E	0.022	0.4	1.112		8 AR&R 20 year, 5 minutes storm, average 182 mm/h, Zone 1
	G4A	0.022	0.15	1.106		7 AR&R 20 year, 25 minutes storm, average 102 min, 1, 2010 1
	Roof 2F	0.022	0.16			7 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
	G3A	0.028	0.2			4 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
F	Roof 2G	0.026	0.19	0.981	0.98	8 AR&R 20 year, 20 minutes storm, average 102 mm/h, Zone 1
F	G2A	0.034	0.24	0.976	0.976	6 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1

#### CHANNEL DETAILS Name

Max Q Max V (cu.m/s) (m/s)

Due to Storm

OVERFLOW ROUTE DETAILS							
Name	Max Q U/S M	lax Q D/S Sa	afe Q 🛛 I	Max D 🛛 🛚 🕅	vlax DxV	Max Width M	ax V Due to Storm
OF L4	0	0.012	0.908	0.025	0.01	4	0.3 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF L3	0	0	0	0	0	0	0
OF L2	0	0	0.408	0	0	0	0
OF L1	0	0.011	0.908	0.024	0.01	4	0.3 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF A5	0	0	0.257	0	0	0	0
OF A4	0	0	0.331	0	0	0	0
OF A3 Basin	0	0	0	0	0	0	0
OF A2	0	0	0.908	0	0	0	0
OF A1	0	0	0.908	0	0	0	0
OF Cat 1B Post	0.087	0.087	0.307	0.098	0.09	2.4	0.94 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF B1 - Outlet	0	0	0.908	0	0	0	0
OF Cat 1A Post	0.001	0.001	0.307	0.017	0.01	0.19	0.32 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF M1 - A6	0	0.006	0.041	0.024	0.01	1.22	0.41 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF A6	0	0	0.42	0	0	0	0
OF C1 - Outlet	0	0	1.41	0	0	0	0
OF Cat 1C Post	0.086	0.086	0.307	0.097	0.09	2.38	0.95 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF C2 - C1	0	0	0.472	0	0	0	0
OF D3 - D2	0	0.012	0.023	0.04	0.02	1.02	0.59 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF D2 - D1	0	0.004	0.023	0.026	0.01	0.64	0.43 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF D1 - Outlet	0	0	1.438	0	0	0	0
OF Cat 2 Post	0.404	0.404	0.307	0.165	0.2	4.72	1.23 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF E1 - D1	0	0.004	0.698	0.018	0	1.82	0.21 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF F4 - F3	0	0.009	0.908	0.023	0.01	4	0.27 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF F3	0	0	0.023	0	0	0	0
OF F2 - Outlet	0.001	0.001	0.982	0.009	0	0.94	0.19 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF Cat 3 Post	0.28	0.28	0.307	0.143	0.17	3.92	1.19 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF G5 - G4	0	0.003	0.023	0.023	0.01	0.57	0.38 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF G4 - G3	0	0.003	0.023	0.023	0.01	0.57	0.39 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF G3 - G2	0	0.002	0.023	0.02	0.01	0.5	0.38 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF G2 - Outlet	0	0	1.431	0.02	0.01	0	0
OF N Cat 4 Post	0.406	0.406	0.307	0.165	0.2	4.72	1.23 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF H2 - Outlet	0	0	1.138	0	0	0	0
OF H3 - H2	0	0.003	0.022	0.025	0.01	0.63	0.43 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF H4 - H3	0	0.005	0.022	0.03	0.01	0.76	0.47 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF J1	0	0	0.336	0	0	0	0
OF Cat 1C Pre	0.098	0.098	0.307	0.102	0.1	2.53	0.96 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF Cat 1A Pre	0.003	0.003	0.307	0.034	0.02	0.39	0.52 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF Cat 1B Pre	0.163	0.163	0.307	0.12	0.13	3.15	1.06 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF Pre North	0.329	0.329	0.307	0.154	0.18	4.45	1.17 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF Post North	0.189	0.189	0.307	0.126	0.14	3.34	1.09 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF N Cat 2 Pre	0.562	0.562	0.307	0.182	0.25	5.14	1.36 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF N Cat 3 Pre	0.315	0.315	0.307	0.152	0.18	4.36	1.16 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF N Cat 4 Pre	0.383	0.383	0.307	0.162	0.2	4.65	1.21 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF Cat South Pre	1.259	1.259	0.307	0.234	0.41	6.45	1.76 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF N Cat Bypass Pre	0.064	0.064	0.307	0.089	0.08	2.1	0.89 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF Cat Bypass 1 Post	0.017	0.017	0.307	0.058	0.04	1.05	0.74 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF N Cat South Post	1.09	1.09	0.307	0.223	0.38	6.18	1.68 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF K1	0	0.07	0.908	0.044	0.03	4	0.61 AR&R 20 year, 25 minutes storm, average 91.7 mm/h, Zone 1
OF G7	0	0	0.307	0	0.00	0	0
OF G6	0	0	0.307	0	0	0	0
OF G5A	0	0	0.307	0	0	0	0
OF G4A	0	0	0.307	0	0	0	0
OF G3A	0	0	0.023	0	0	0	0
OF G2A	0	0	0.307	0	0	0	0
-	-	-		-		-	

DETENTION BASIN DETAILS				
Name	Max WL	MaxVol	Max Q Total	Max Q Max Q Low Level High Level
A3 Basin	1.31	5.6	0.052	-
CONTINUITY CHECK for AR&R 20 Node	) year, 25 mi Inflow	nutes storn Outflow	n, average 9 Storage Ch	
	(cu.m)	(cu.m)	(cu.m)	%
L4 L3	8.36 17.31			
L2	30.76			
L1 A5	45.2 71.44			
A3 A4	57			
A3 Basin	-623.6			
Line A - HG18 Line A - STC18	90.42 120.98			
A2	110.38			
A1 Cat 1B	134.05 139.89			
B1	0.33			
Cat 1A M1	0.33 11.55			
A6	20.7			
Roof 5A	37.74			
C1 Cat 1C	64.5 64.5	64.5 64.49		
Roof 5B	23.04	23.09	0	
C2 Roof 1C	24.47 89.54			
D3	108.75			
HG30A	108.67			
STC18 D2	108.7 189.19			
D1	304.46			
Cat 2 Roof 1A	304.52 42.39			
E1	110.12			
Roof 2C F4	75.92			
F4 F3	89.18 151.86			
Line F - HG18	151.84	151.85		
Line F - STC9 F2	151.85 211.12			
F1	210.97			
Cat 3 Roof 2B	211.1 49.31			
Roof 2A	47.71			
Roof 3D	18.38			
G5 G4	132.84 167.29			
G3	201.56			
Line G - HG18 Line G - STC 9	201.53 201.53			
G2	243.28			
G1 Dummy	243.22 326.59			
Cat 4	326.54			
Roof 3C	10.2			
Roof 3B Roof 3A	10.2 12.21			
Roof 3E	11.02	11.02	0	
H2 H1	83.33 83.3			
Roof 3F	20.54			
H3 Roof 3G	67.28 27.17			
H4	38.71			
Roof 5C	15.52			
Roof 5D J1	35.43 32.34			
Roof 5E	6.44			
Roof 5F N Cat 1C Pre	6.29 73.28			
N Cat 1A Pre	2.38			
N Cat 1B Pre N Pre North	122.29 246			
N Pre North N Pre North Total	246			
N Post North	216.74			
N Post North Total N Cat 2 Pre	216.3 420.66			
N Cat 3 Pre	235.73	235.73	0	0
N Cat 4 Pre N Cat South Pre	284.43 940.82			
N Cat South Total	940.82	940.82		
N Cat Bypass 1 Pre	48.05			
N Cat Bypass 1 Post N Cat South Post	12.29 842.15			
N Cat South Post Tot	842.17	842.17	0	0

K1	17.57	-27.1	0	254.2
G7	44.03	44.02	0	0
G6	73.16	73.15	0	0
N Caltex	0	0	0	0
Roof 1B	62.67	62.61	0	0.1
N Roof 1D	64.68	64.65	0	0.1
N Roof 2D	33.79	33.83	0	-0.1
G5A	37.81	37.76	0	0.2
N Roof 2E	16.34	16.39	0	-0.3
G4A	20.41	20.38	0	0.1
N Roof 2F	16.3	16.34	0	-0.2
G3A	20.39	20.36	0	0.2
N Roof 2G	19.76	19.69	0	0.3
G2A	24.64	24.76	0	-0.5

Run Log for 366163 170622 Wickham Woolstores Final Current.drn run at 11:42:02 on 3/7/2017{\rtf1\ansi\deff0{\colortbl;\red0\green0\blue0;\red255\green0\blue0;}No water upwelling fi \par }



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